

# QPS Engineering Design

Presented by B. Nelson for the QPS design team

QPS PVR  
April 24, 2001  
ORNL



# Presentation Outline

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- **Baseline parameters**
- **Stellarator core configuration**
  - **Modular coils, VF/TF coils, structure, vacuum tank**
  - **What are the requirements?**
  - **What is the design concept?**
  - **How do we plan to build it?**
- **Summary and plans for CDR**

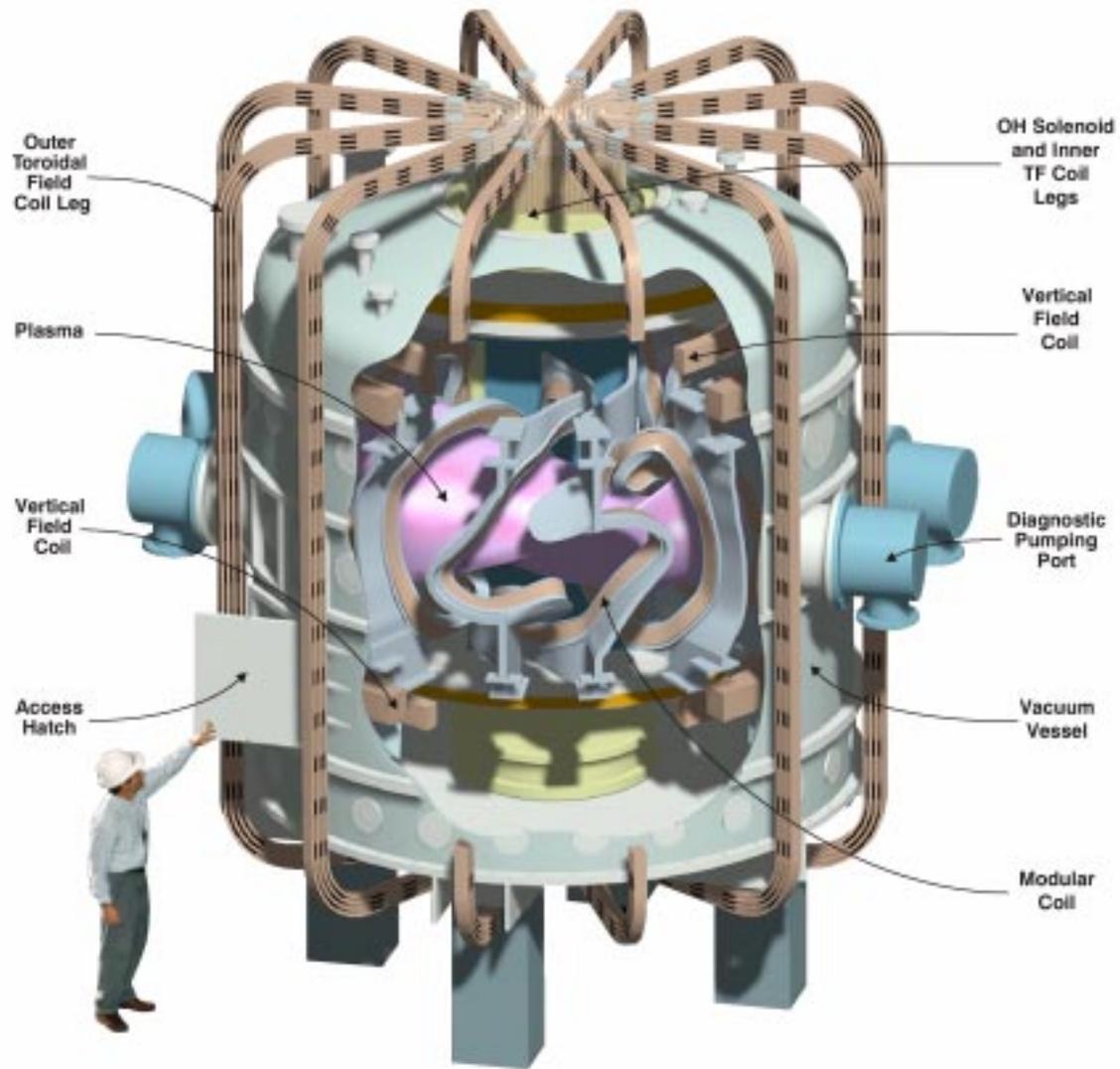
# Baseline parameters for QPS design

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- **Moderate size and field**
  - $\langle R0 \rangle \sim 0.90$  m
  - $\langle a \rangle \sim 0.35$  m
  - $B0 = 1$  T
- **Factory assembled unit desired, consisting of modular coils, VF and TF coils, and structure**
  - **Minimum cost is essential**
  - **Uses existing power supplies, cooling system, diagnostics, vacuum pumps, ECH system, etc.**

# QPS Concept

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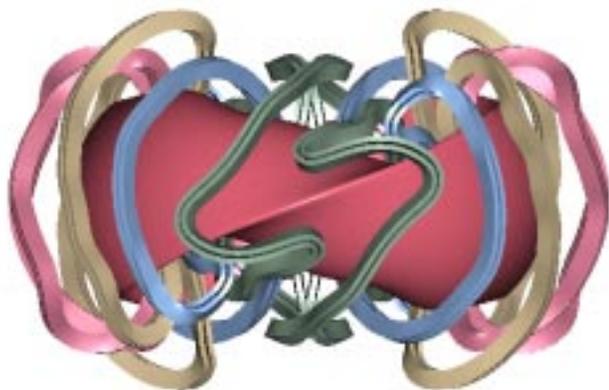
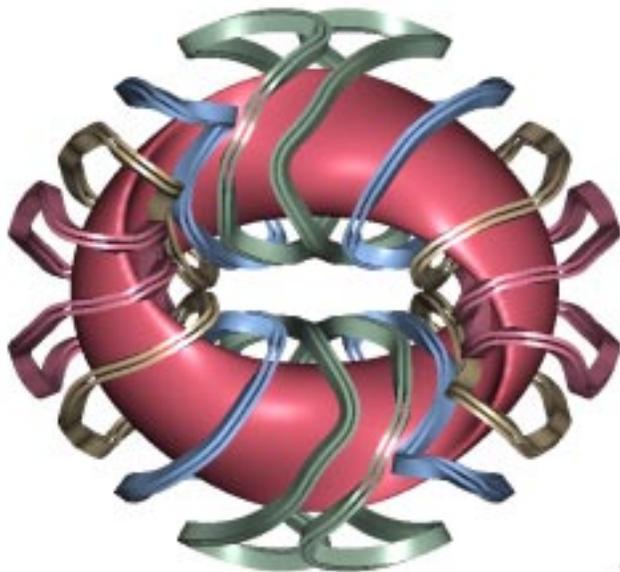
# Modular coil requirements

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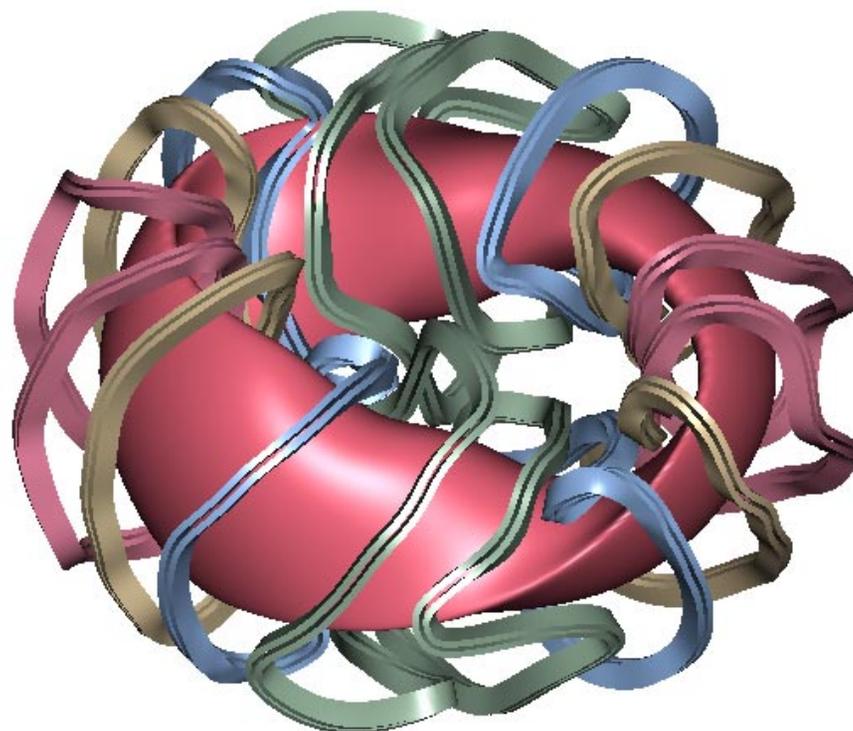
- **Meet performance requirements**
  - 1 T with 0.5 s flattop
  - 10 minute rep rate (5 minute rep rate for shorter pulses)
- **Provide flexibility**
  - Independent control of modular and PF coils provided
  - Variable background TF field +/- 0.15 T
- **+/- 1 mm assumed for winding accuracy**
- **Coil structure should maximize access for heating and diagnostics**
- **Limit conductor current and voltage drop to match existing power supplies**

# Modular coil configuration

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**Coil set 0213b2 (as scaled)**  
 **$R_0 = 0.90$  m,  $a = 0.35$  m**



# Modular Coil Geometry

Cross section shape and size depends on details of bending radius, twist, coil-coil spacing, coil-plasma spacing



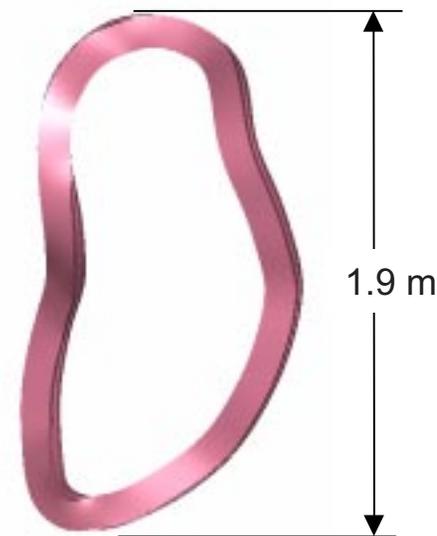
Coil 1



Coil 2

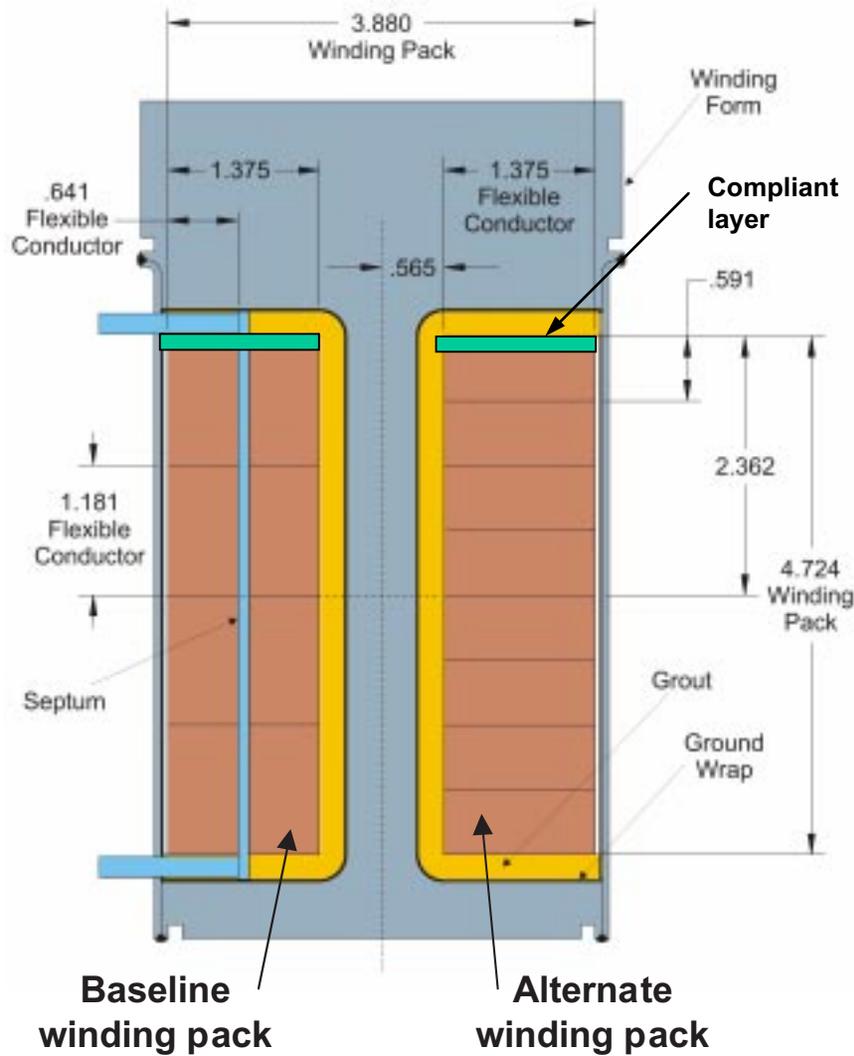


Coil 3



Coil 4  
bean  
section

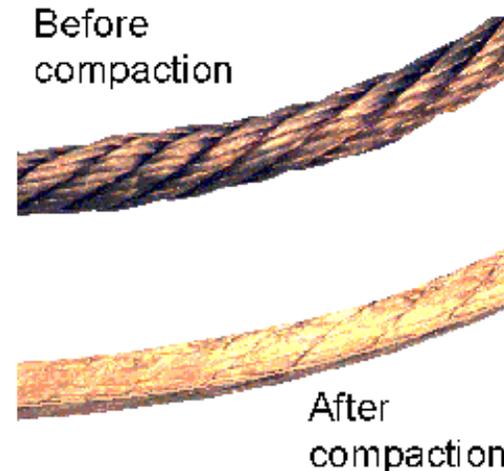
# Modular coils wound with flexible cable directly on coil structure



## Parameters:

- ¥ Coil Envelope ~ 2 x 120 x 34 mm
- ¥ Current / Coil = 337-kA @ 1 Tesla
- ¥ Number of Turns = 16
- ¥ Avg length per turn = 5.07 m
- ¥ Nominal current / turn = 21.1 kA
- ¥ Conductor Size = 16 x 30 mm
- ¥ Heat removed via gas-cooled septum
- ¥ Net Current Density ~ 8-kA/cm<sup>2</sup>
- ¥ Total peak power ~ 45 MW

## Flexible cable used to wind coil



# Modular coil manufacturing sequence

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- Continuous support for strength and accuracy of windings
- Castings repeated four times for each coil type



Rough casting



Features are machined, winding cavity grouted



Conductor wound directly into structure



Side plates welded to structure

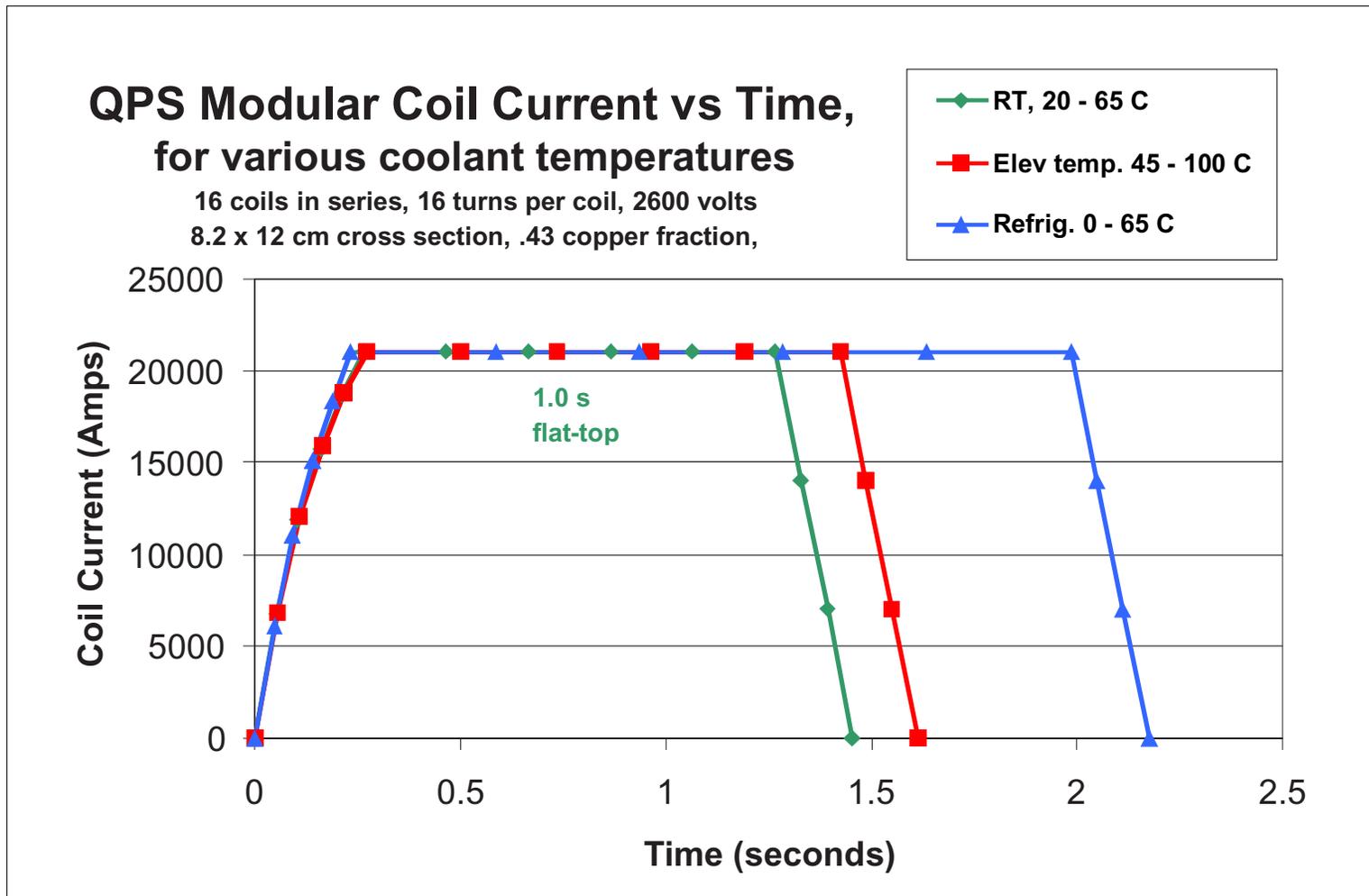


# Ramp rate and flat-top considerations

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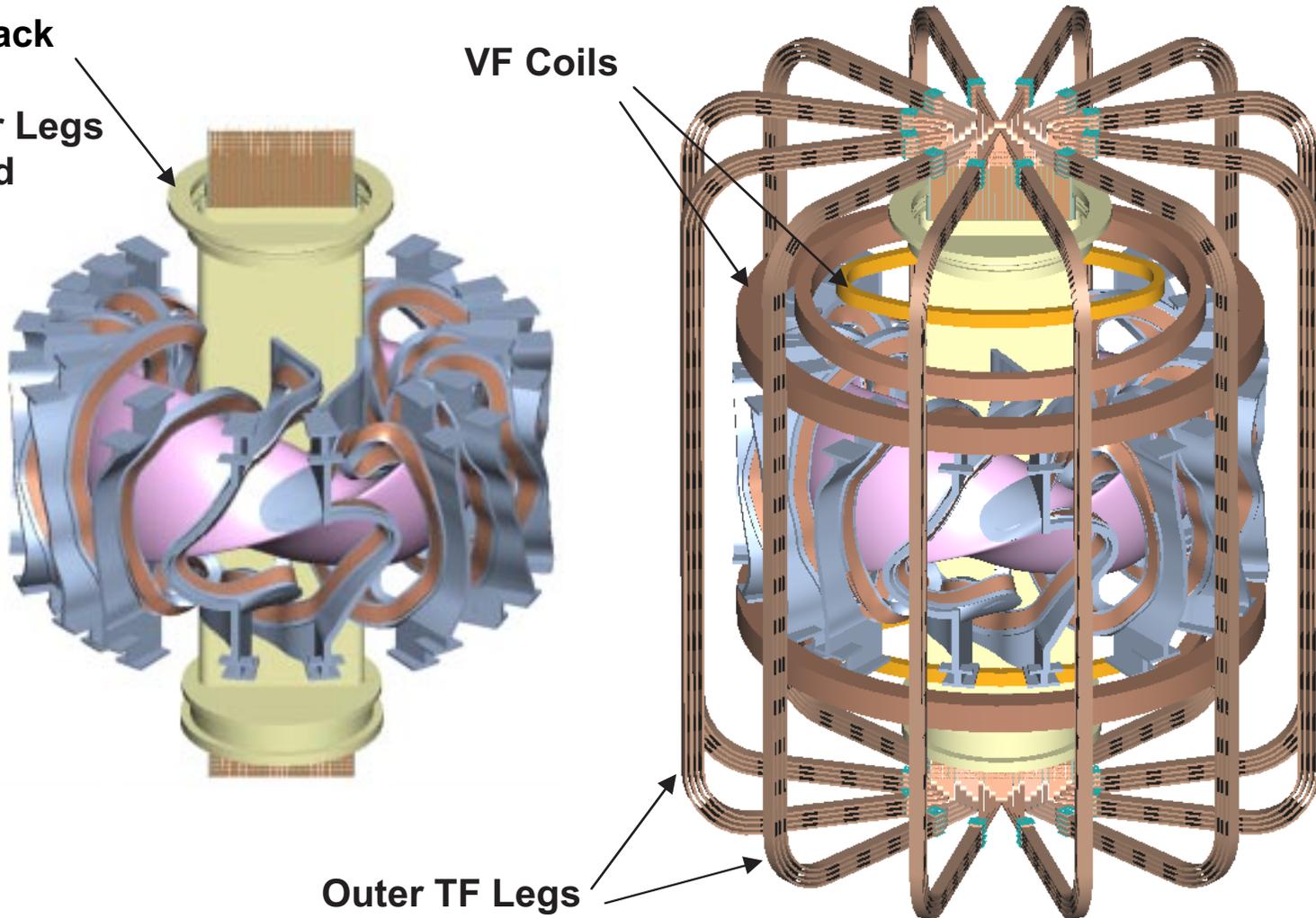
- **Temperature limits**
  - Max temp depends on epoxy used, RT cure epoxy limited to ~ 65C, heat cured epoxy can go to 100C
  - Min temp depends on thermal isolation of coils and compatibility with plasma vacuum
- **Power supply limitations**
  - 4 solid state modules rated at 650 V, 30 kA pulsed (7.5 kA continuous)
  - 3 solid state supplies rated at 625 V, 15 kA pulsed (~ 3 kA continuous)
- **Eddy current decay time in structure**
  - Error fields not completely symmetrical due to casting variations
  - I-Beam castings have <10 ms time constant

# Coil parameters, power supply, cooling temp. determine pulse waveform and flat-top time



# TF and VF coils

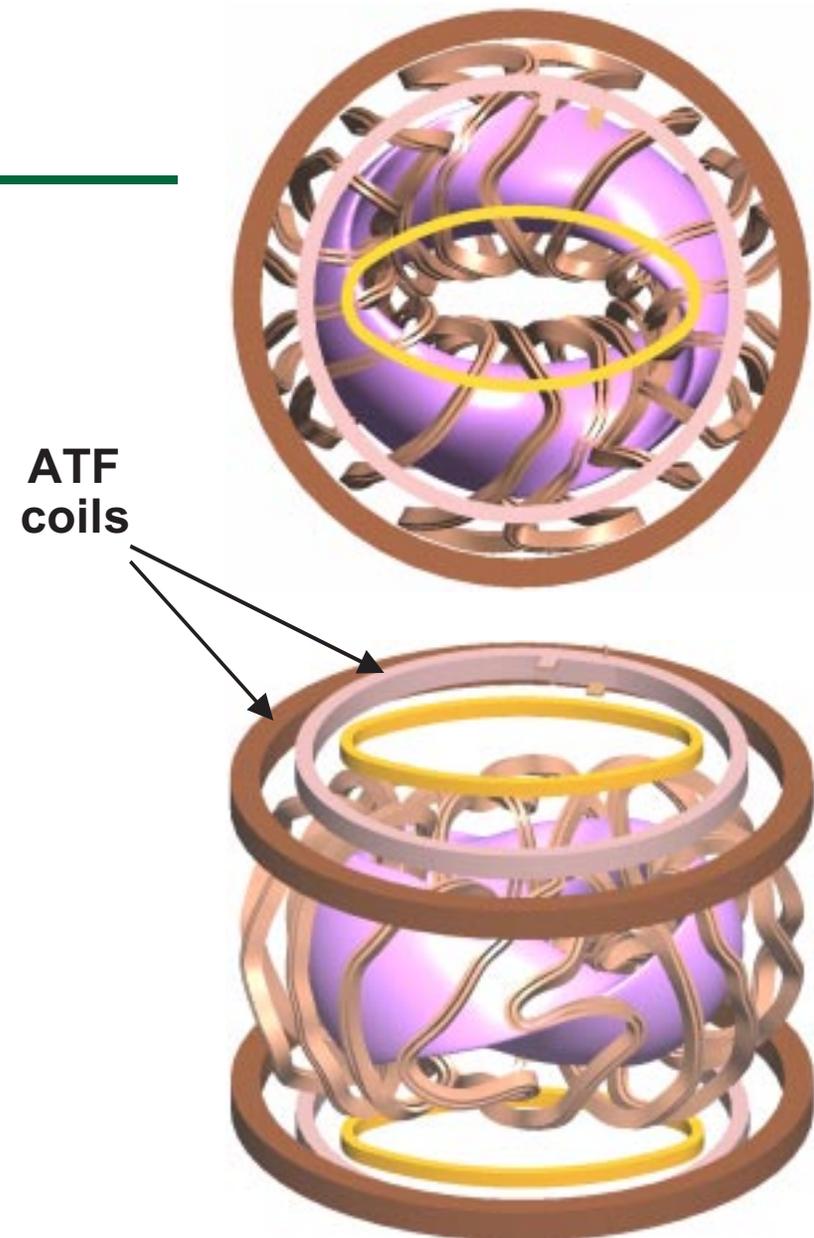
**Center Stack  
Includes:**  
¥ TF Inner Legs  
¥ Solenoid



## VF / Trim Coils

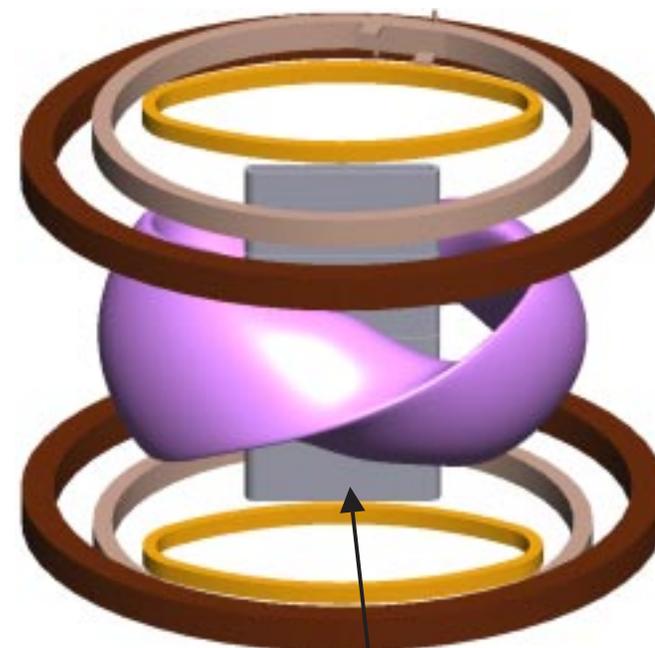
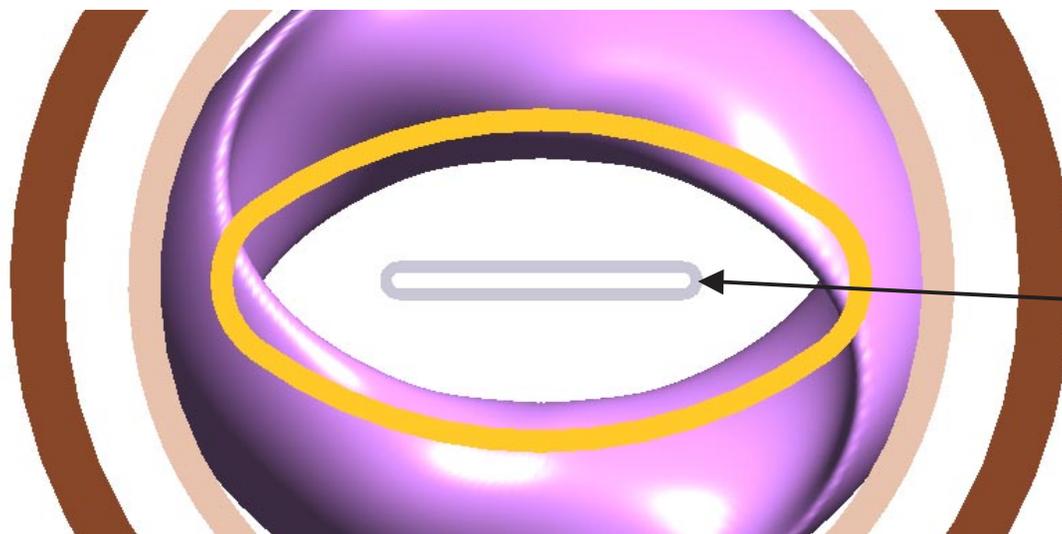
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- 3 pairs of VF coils are included in design
- Planar coils are assumed
- Combination of existing ATF coils and new coils
- Elliptical shape for mid/inner VF coil pair is planned



## OH solenoid / return coils

- Central solenoid is limited to oblong shape by modular coils
- Plan to use VF / trim coils for outer return coils
- Present configuration limited to  $\pm 0.15$  V-S by power supply
- Forces will require ties across winding

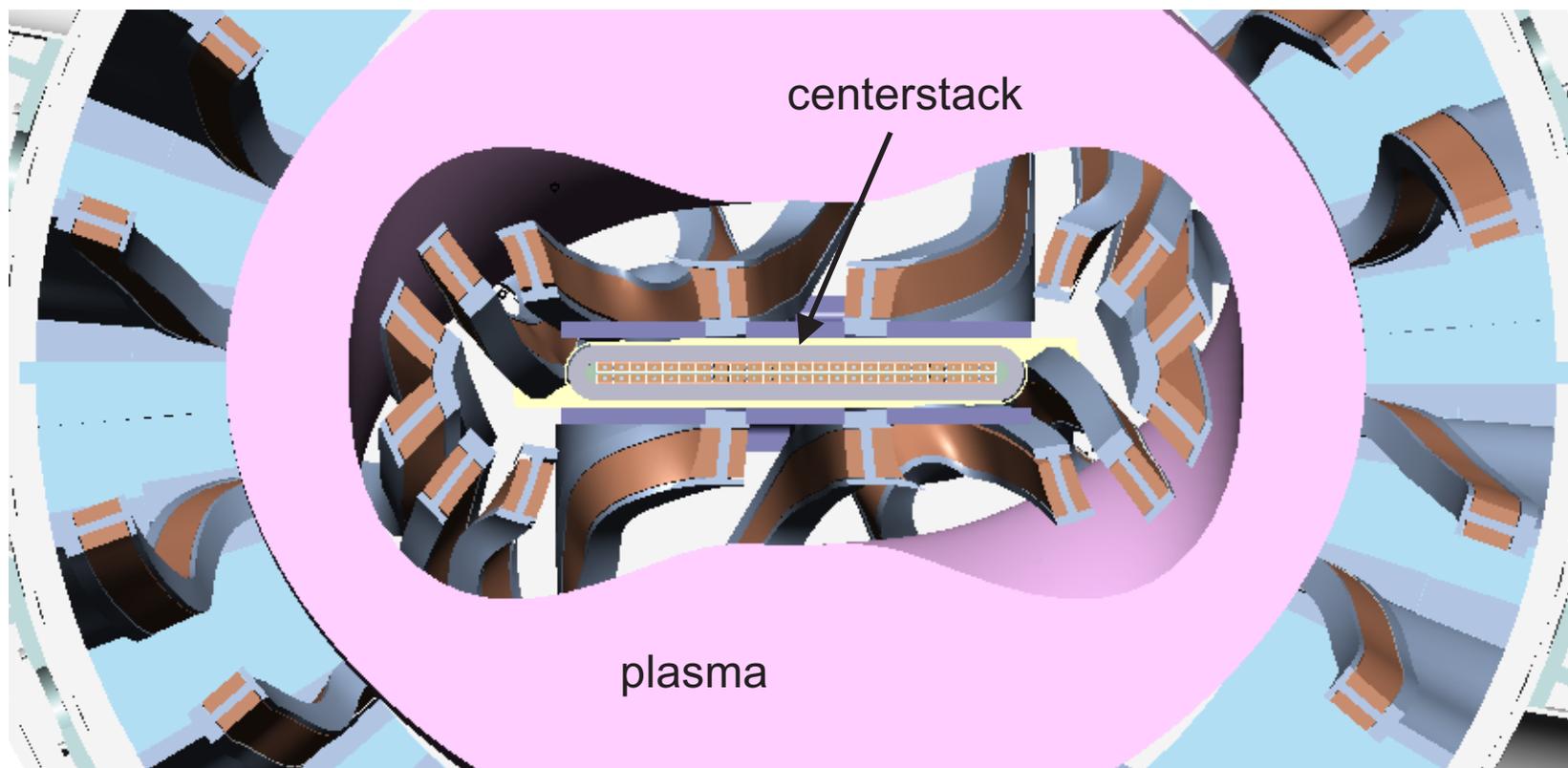


OH  
solenoid

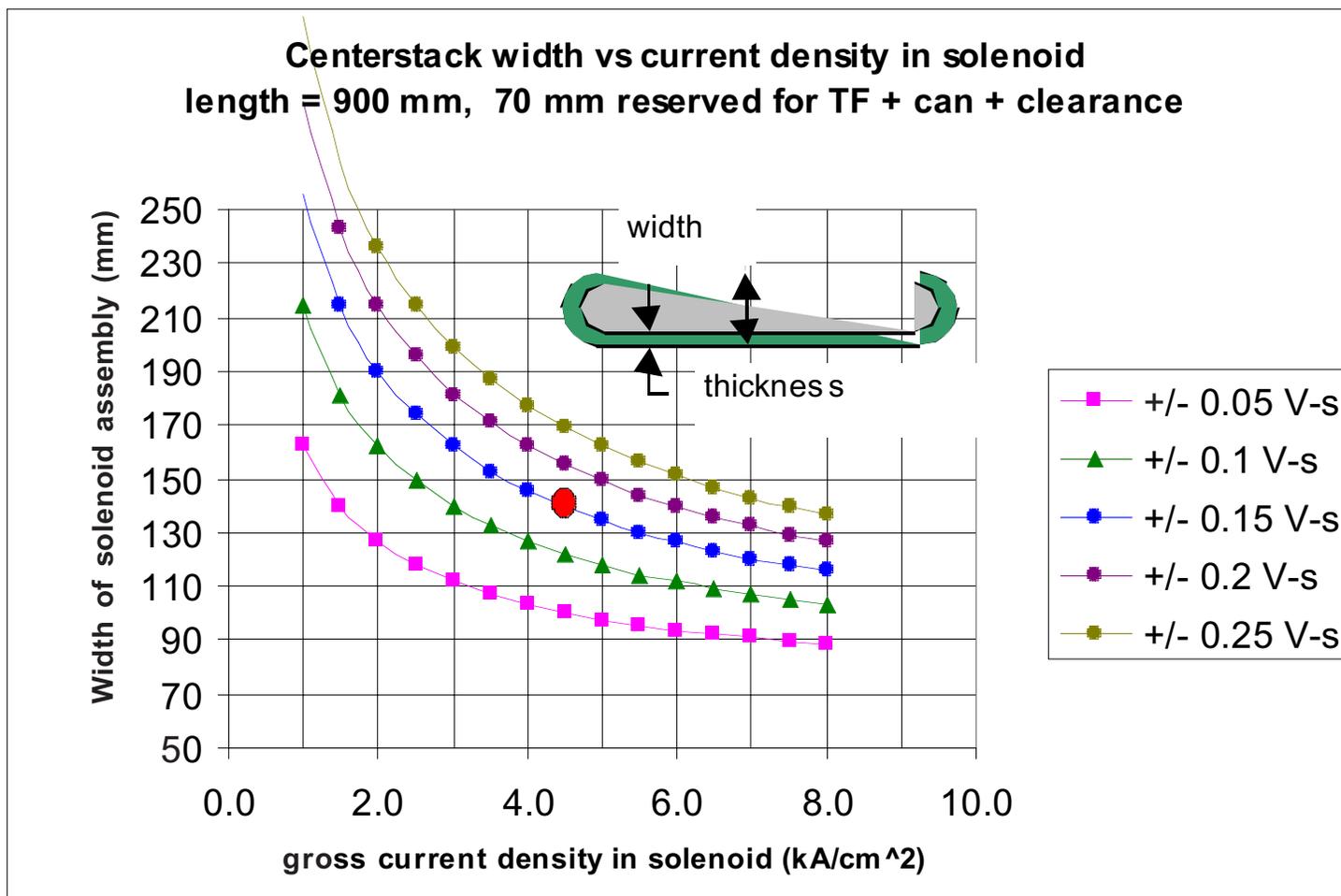
## Centerstack occupies oblong space

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- Limited room for TF coils, OH solenoid and vacuum casing
- Available clear vertical bore is ~ 14 x 90 cm

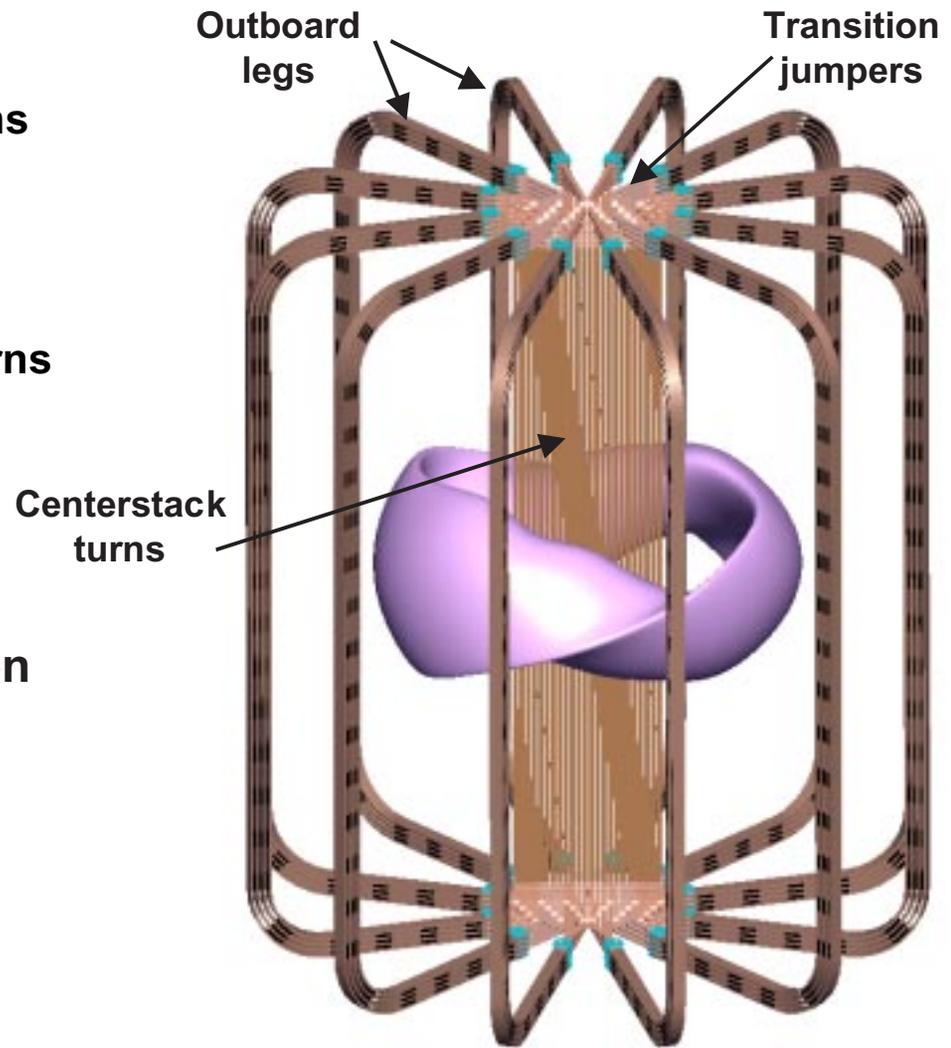


# What space is needed for solenoid?

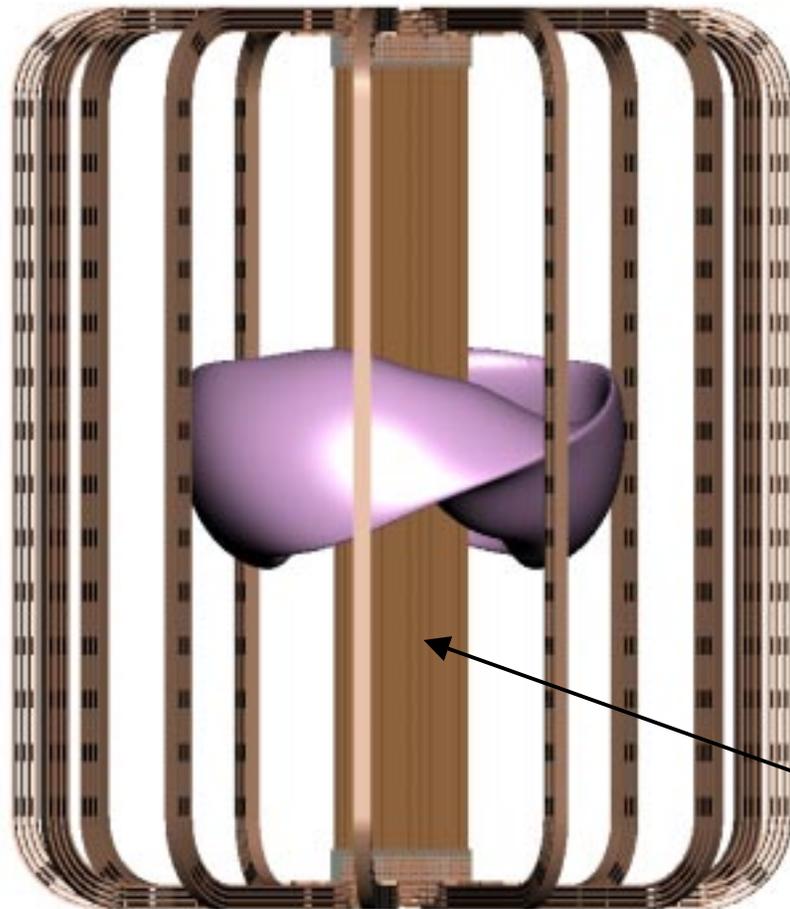


# TF coils

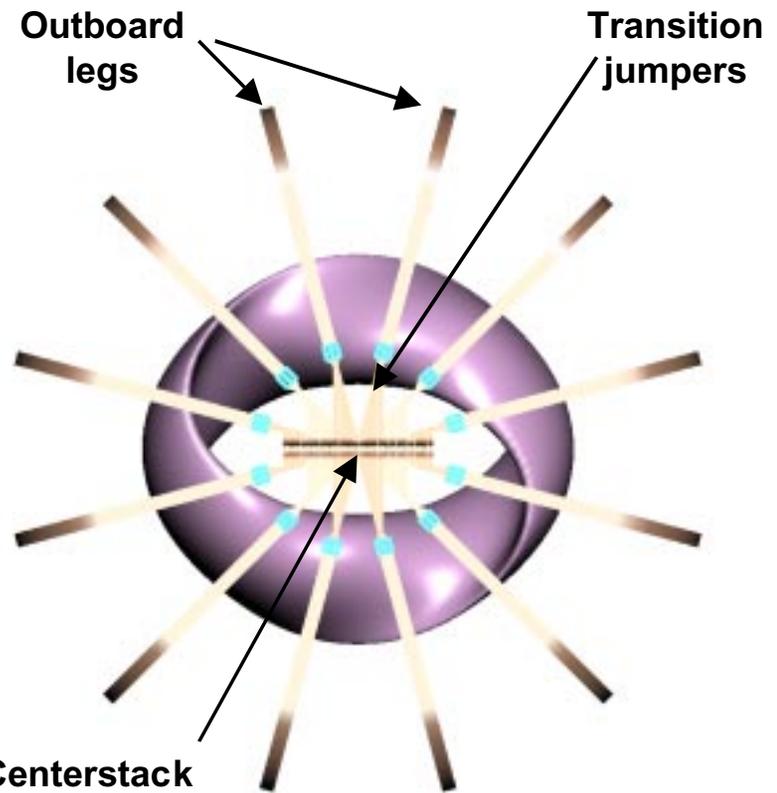
- **48 turns**
  - 1.5 x .75 in. centerstack turns
  - 3.5 x .75 in. outboard
- **+/- 0.15 T (14 kA / turn)**
  - ~2100 A/cm<sup>2</sup> centerstack turns
  - ~ 850 A/cm<sup>2</sup> outboard
- **12 return leg bundles**
- **Odd shape requires transition jumpers at center stack**
- **Stellarator symmetry is preserved**



# TF coils (2)



**Elevation view**



**Plan view**

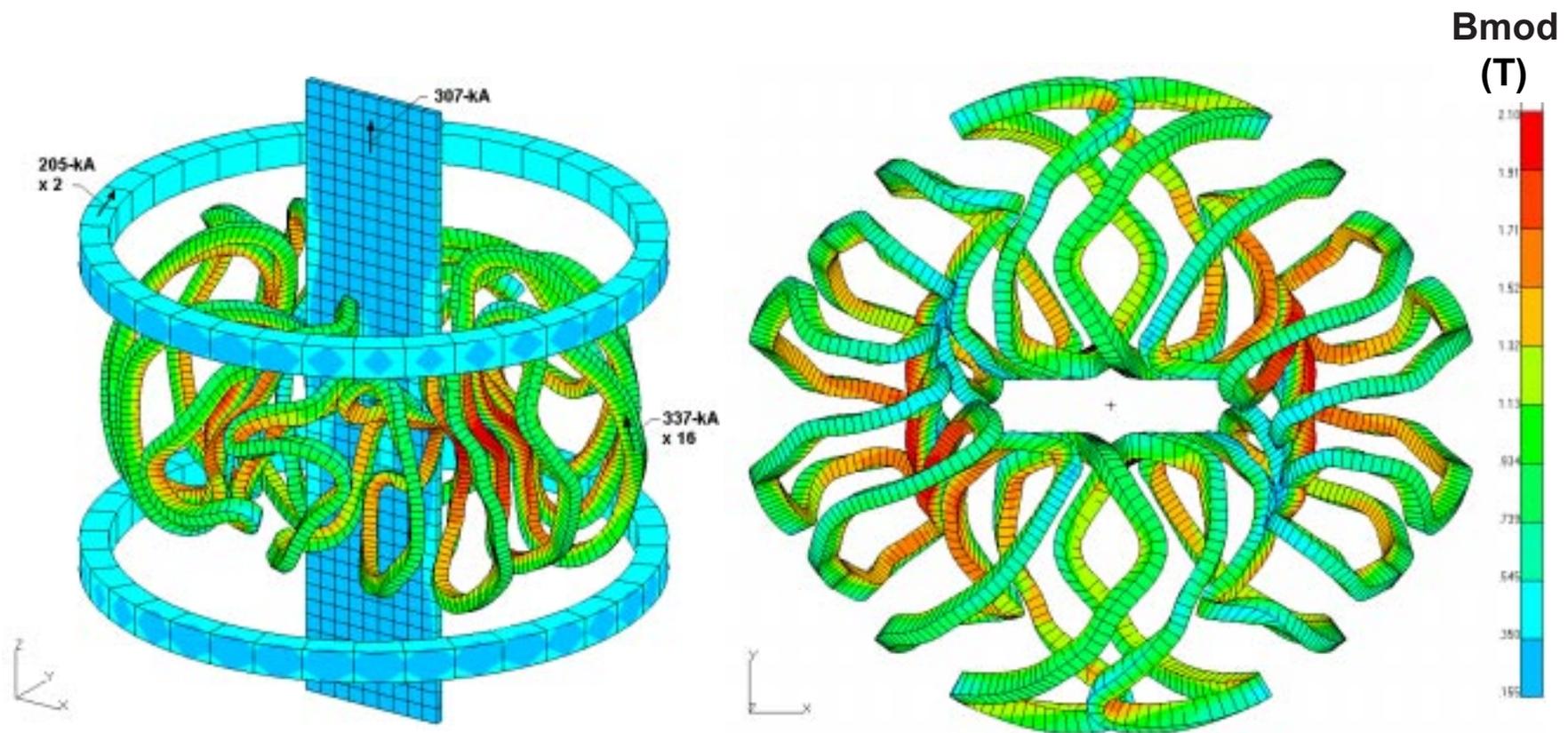
## Coils match up with existing power supplies

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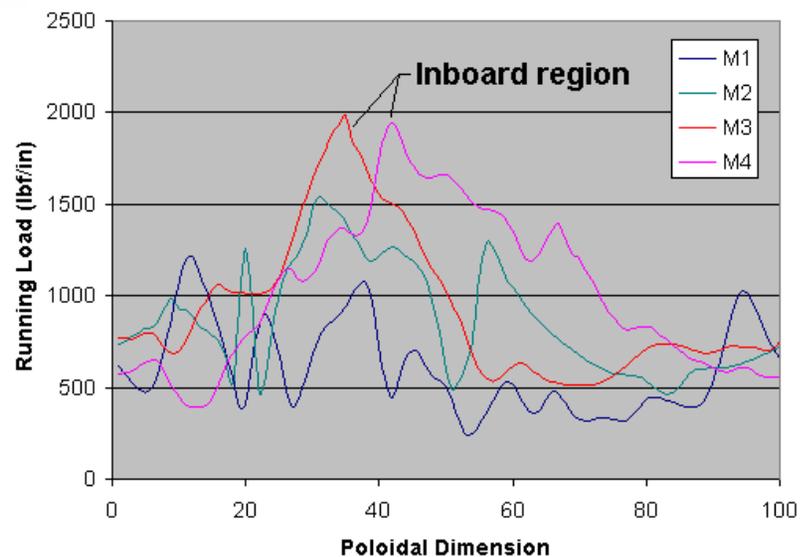
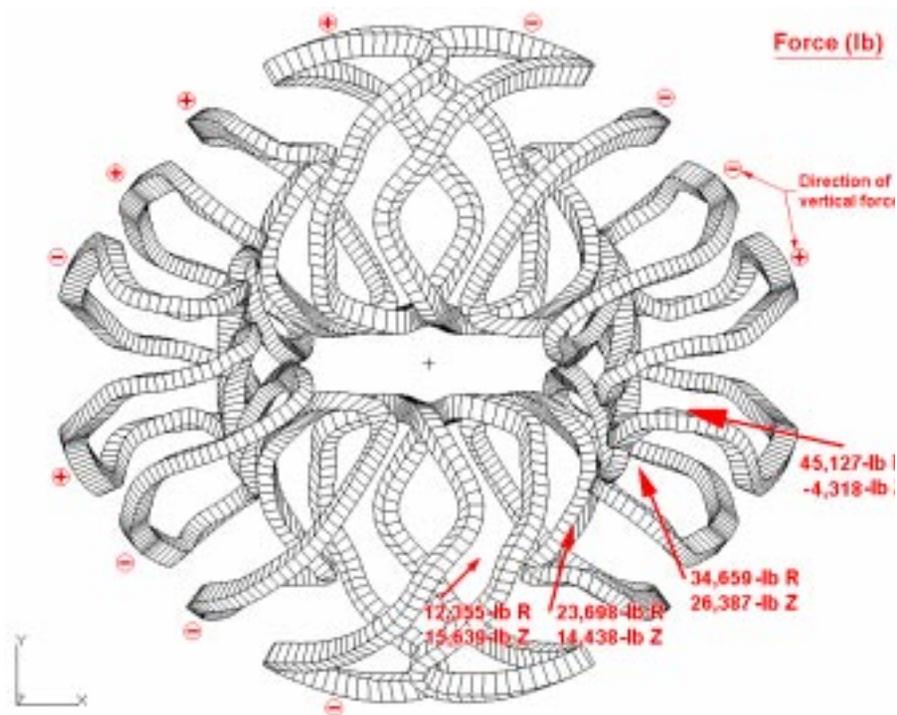
Coil Set	Power Supply
Modular Coils, 4 groups of 4 coils	Existing ATF helical field power supplies, 4 each 650 V open circuit voltage, 30 kA pulsed current
OH solenoid 1 solenoid	Existing ATF VF coil power supply 625 V, 15kA pulsed
Mid PF coils 1 pair	Existing LCTF power supplies x 2 12 V, 25 kA
Outer PF coils 2 pairs	Existing ATF VF coil power supply 625 V. 10 kA pulsed rating
TF coils 1 circuit, 48 total turns	Existing ATF VF coil power supply 625 V. 15 kA pulsed rating

# Magnetic field distribution from all coils

$B_{max}/B_0 = 2.1$ , with external TF field of  $-0.06\text{T}$



# Modular coil forces

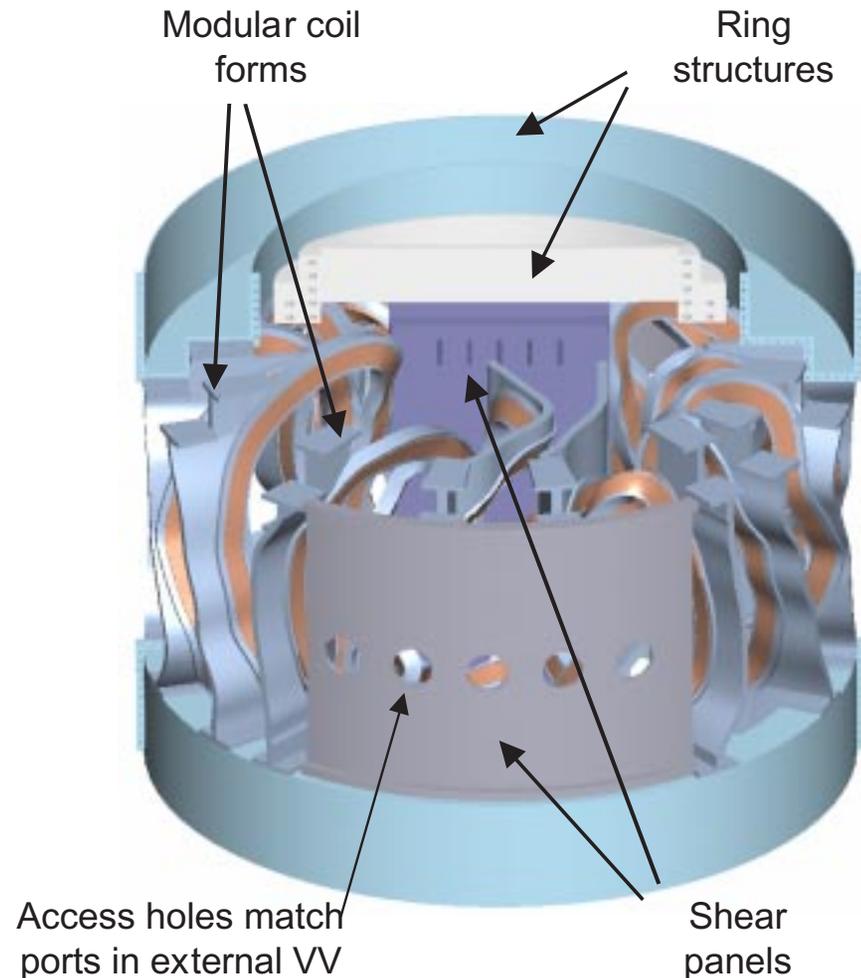


**Max centering load = 45 kips**

**Max running load = 2000 lbs/in**

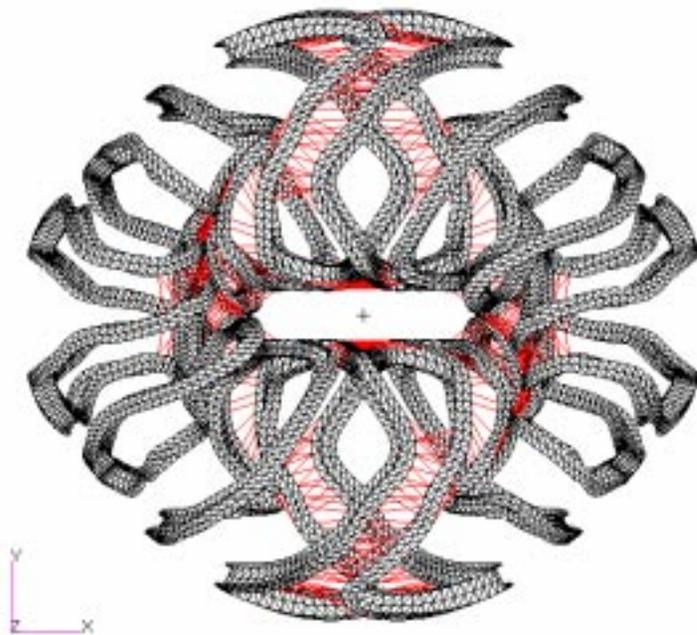
# Machine Structure

- Modular coil winding form provides primary structure
- Coil forms connected to VF coil ring structures and inboard shear panels
- VF ring structures connected with shear panels for twisting and separating forces
- Coil-to-coil structure is more efficient and will be pursued during conceptual design

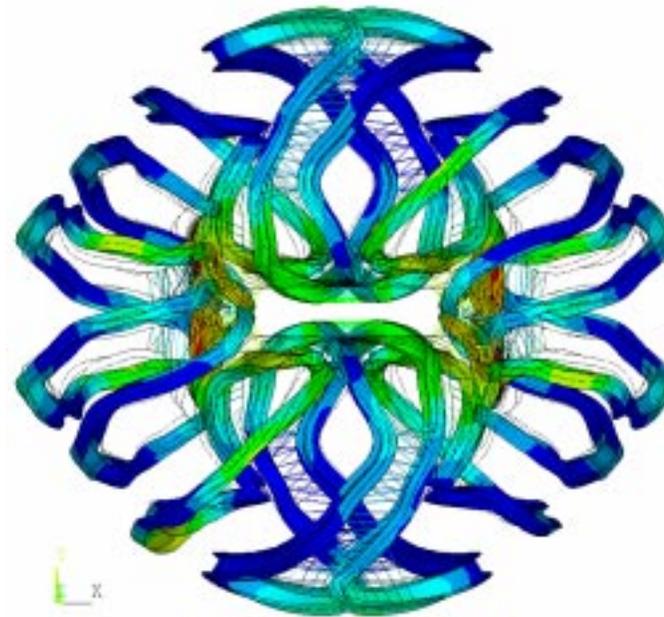


# Modular Coil Structural analysis

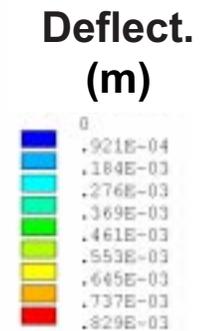
- Coil-to-coil structure shown is sufficient to limit maximum deflection to less than 1 mm



Structural FEA model

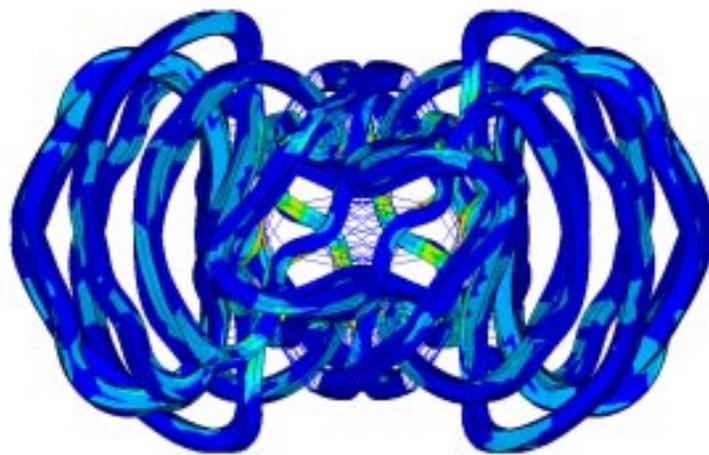


Deflections under load

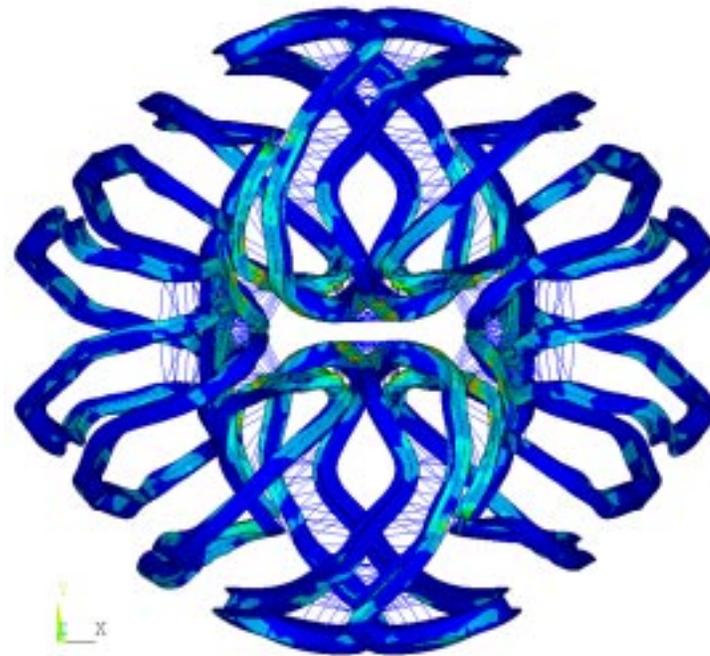


# Stress in modular coil structure

- Stresses limited to ~ 200 MPa (in local regions)
- Stress in most areas < 100 MPa

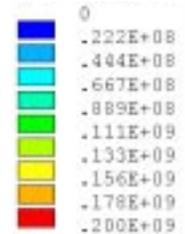


Stress distribution, elev.  
view



Stress distribution, plan  
view

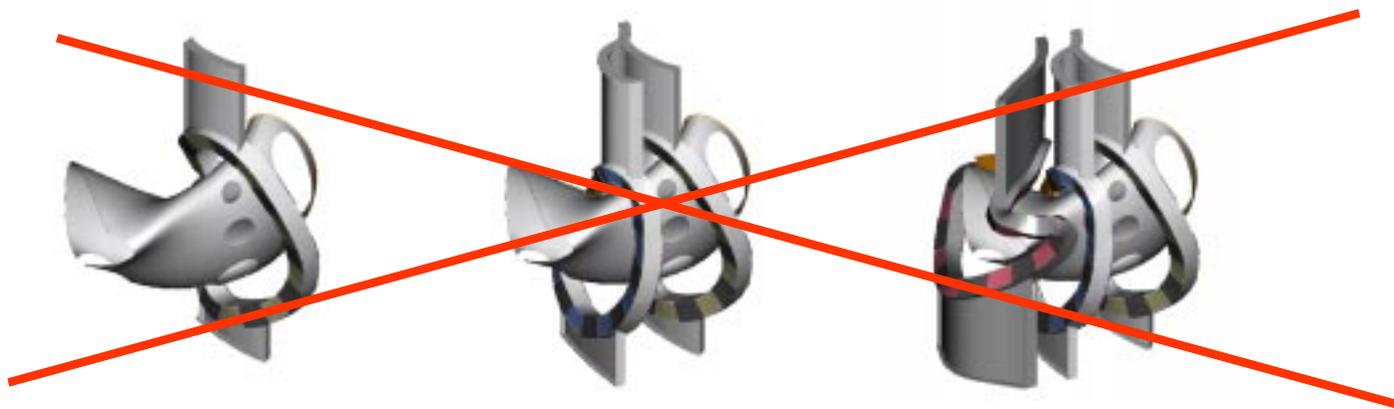
Stress  
(MPa)



## QPS will use external vacuum vessel

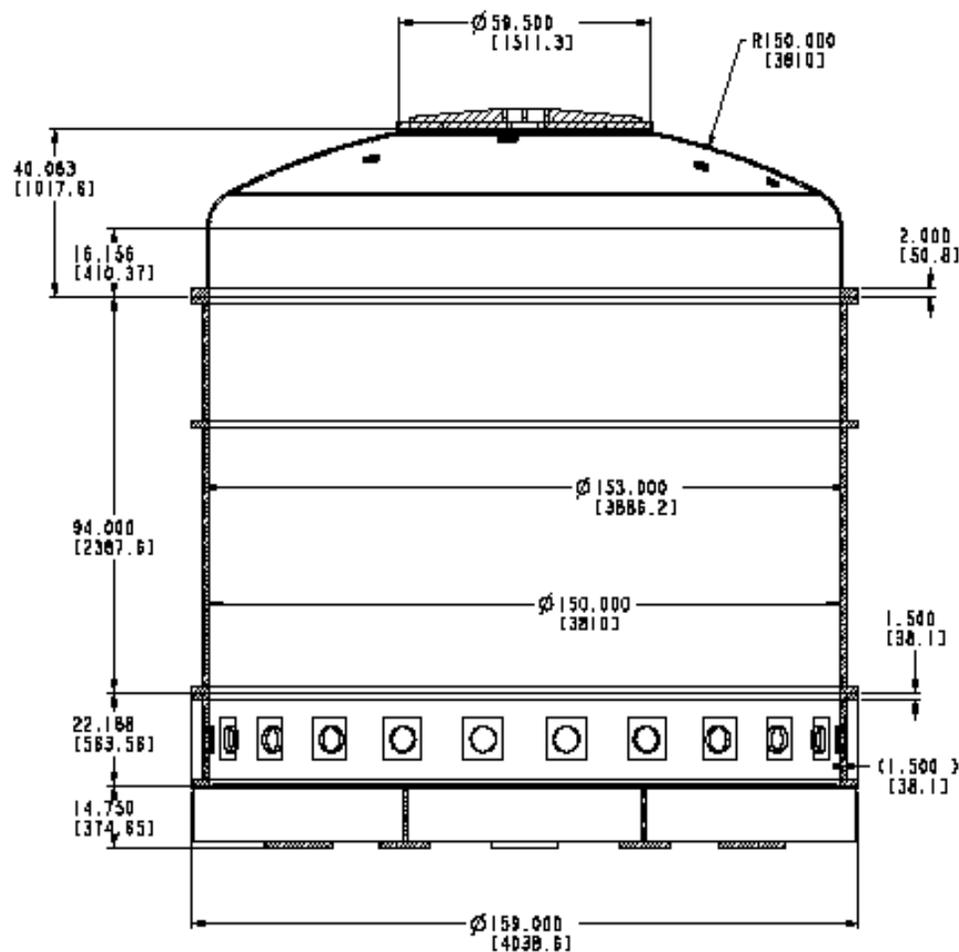
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- **Eliminates complex vacuum vessel fabrication**
- **Provides maximum distance from coils to plasma for greater shape flexibility — e.g. larger plasma or shifted position**

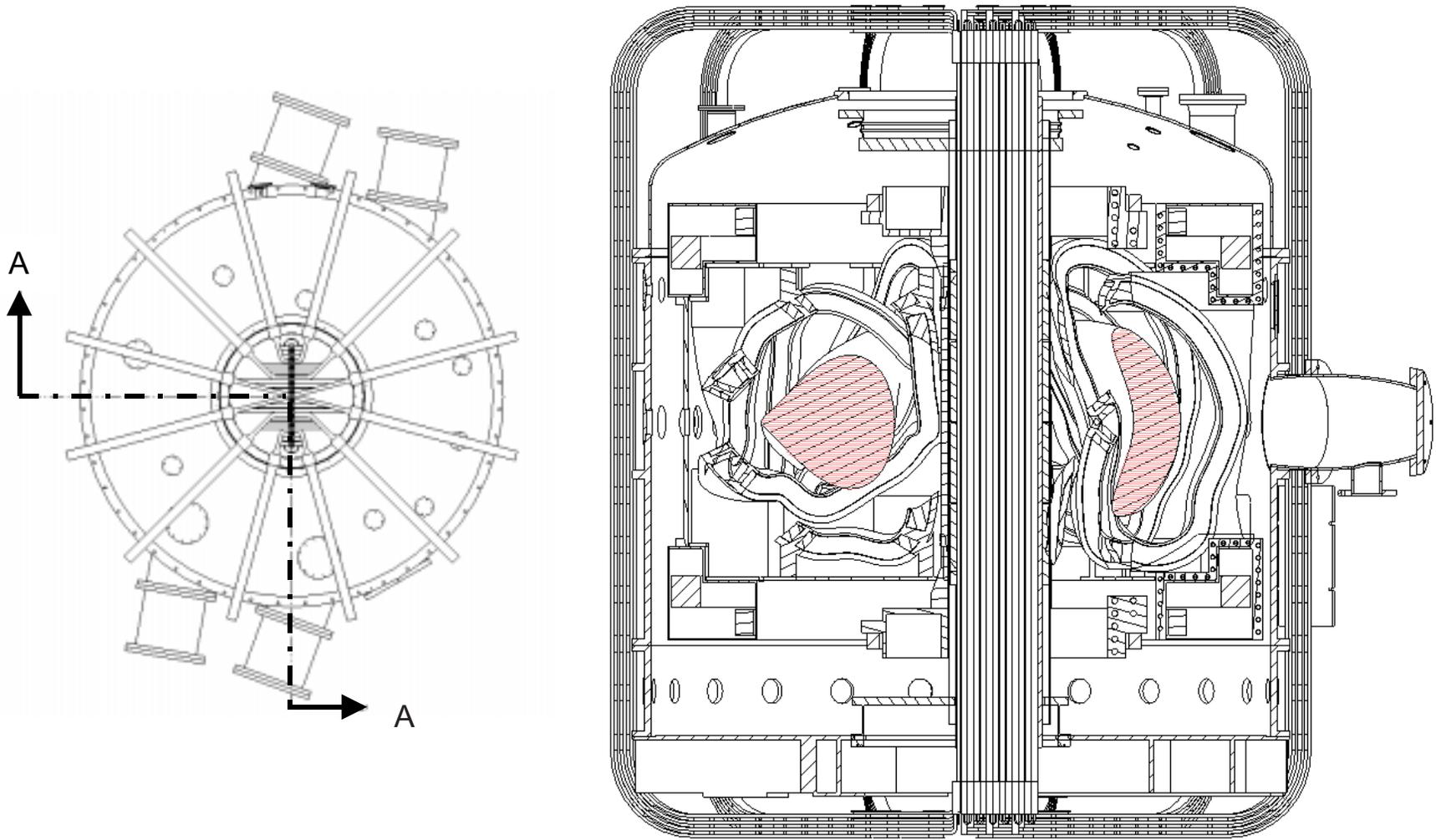


- **Provides more flexibility for structure, since coils do not have to be manipulated over internal vacuum vessel**
- **Bell jar exists (vessel used for ORMAK experiment)**

# Existing bell jar vacuum vessel



# QPS assembly fits within existing bell jar



Section A-A

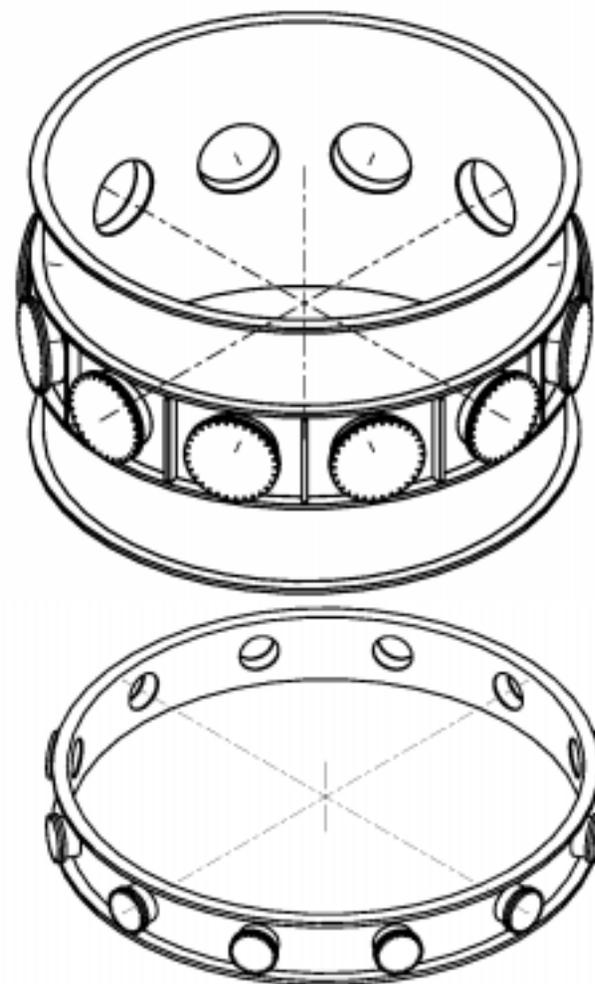
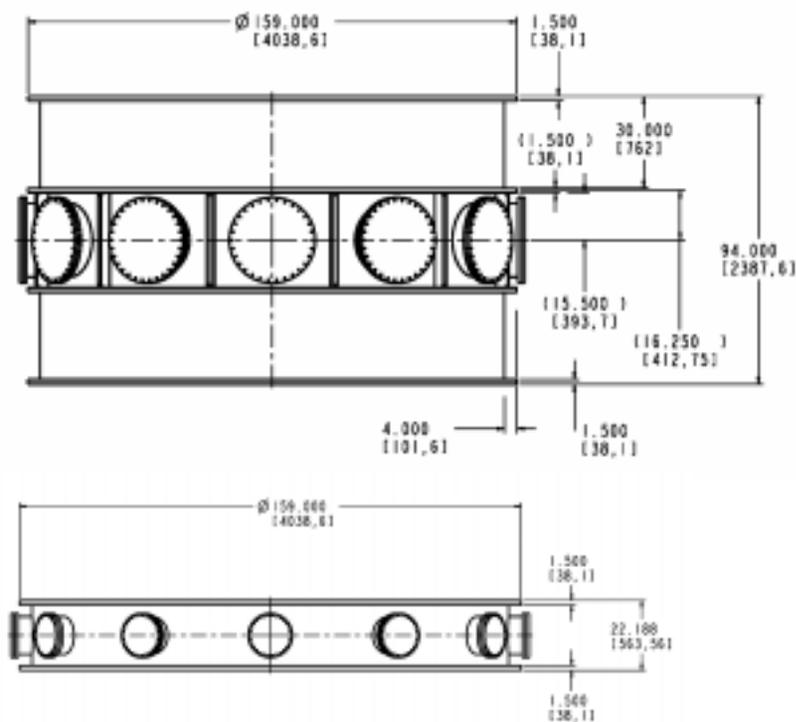
# External vacuum vessel requirements

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- **Clean:**            **bake-able to 150 C (need double seals)**  
**Minimum oxide buildup on inside of tank**
- **No leaks:**      **Integrated leak < 1e-5 torr-l/s**  
**Base pressure < 1e-8 torr for impurities**  
**Base pressure < 1e-7 for H**
- **Can be re-sealed easily after major opening**
- **Time constant issues may require replacement of aluminum spool pieces with stainless steel**
-

# New 304L spool pieces *will* replace aluminum

- Fewer, larger ports
- Lower spool piece could be welded to base to eliminate seal

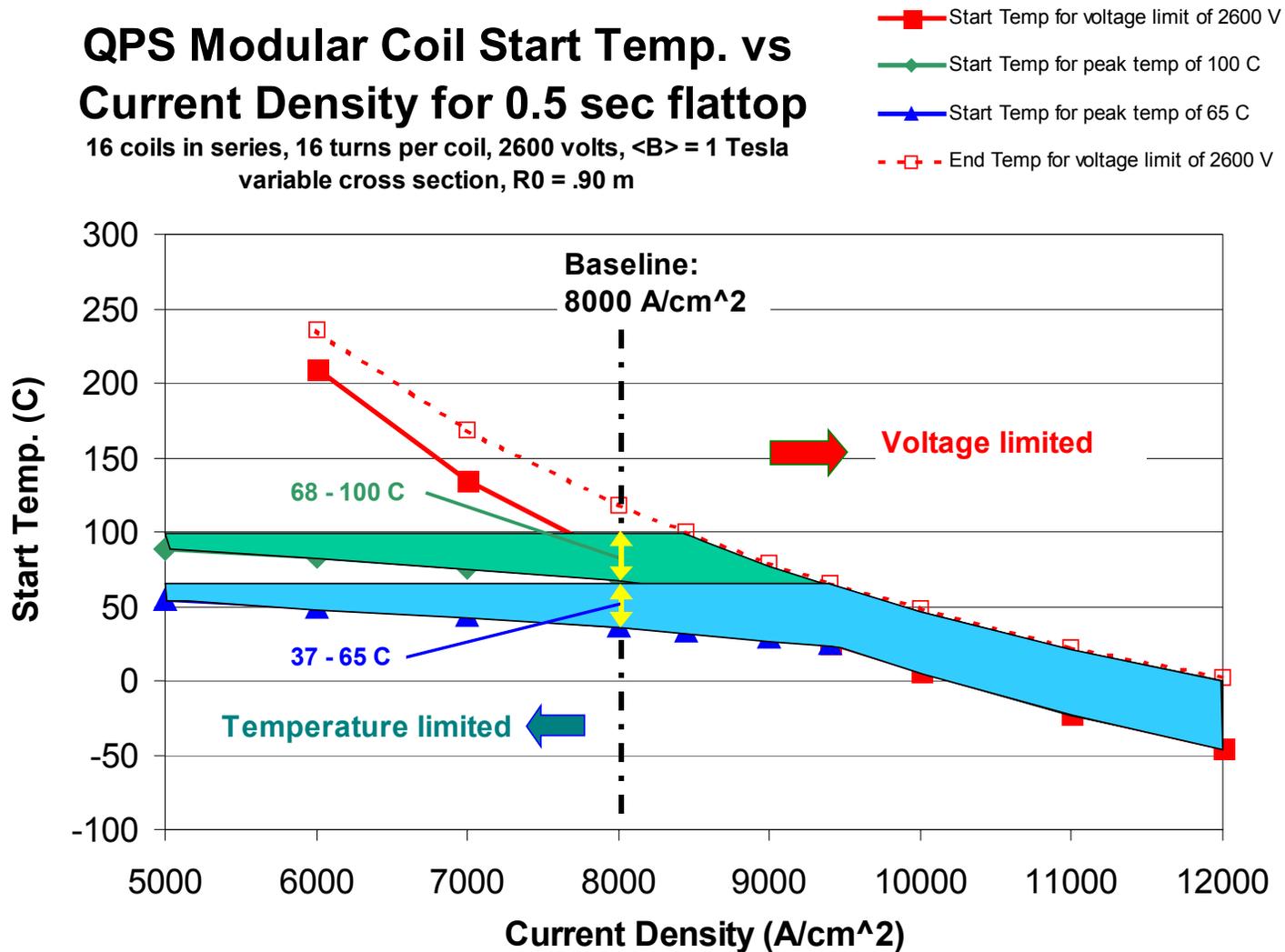


# **Modular coils face the plasma so the coil operating temperature is important**

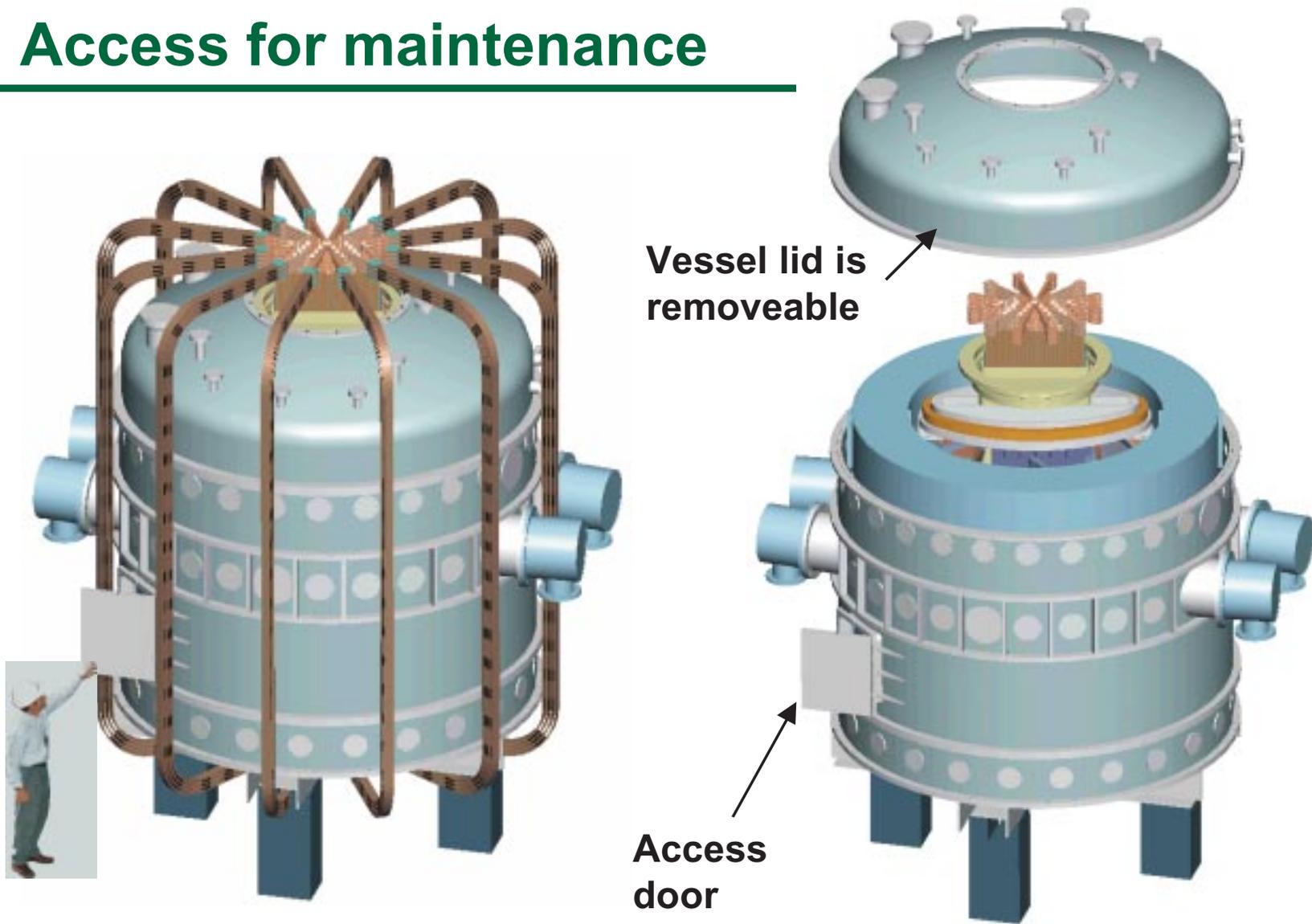
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- **Temperature limited by:**
  - Epoxy in winding
  - Coil resistance and power supply voltage limits
- **Epoxy temperature depends on curing temperature:**
  - Room temperature cure epoxy limited to 65C
  - Elevated temperature cure epoxy limited to ~ 100C
- **Total voltage drop in coils must remain below 650 volts for each coil circuit or 2600 V total**
- **Current density determines temperature rise ( $\propto J^2$ ) and voltage drop ( $\propto J$ ), but voltage is also a function of temp.**

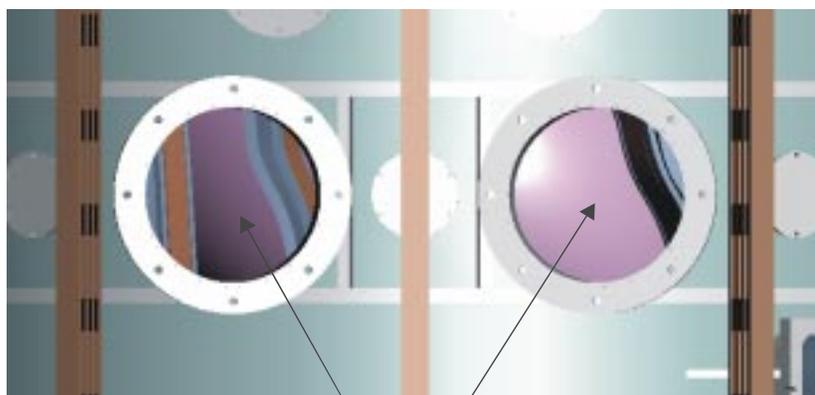
# Baseline current density, 8 kA/cm<sup>2</sup>, does not push voltage or temp limits for 0.5 s flattop



# Access for maintenance



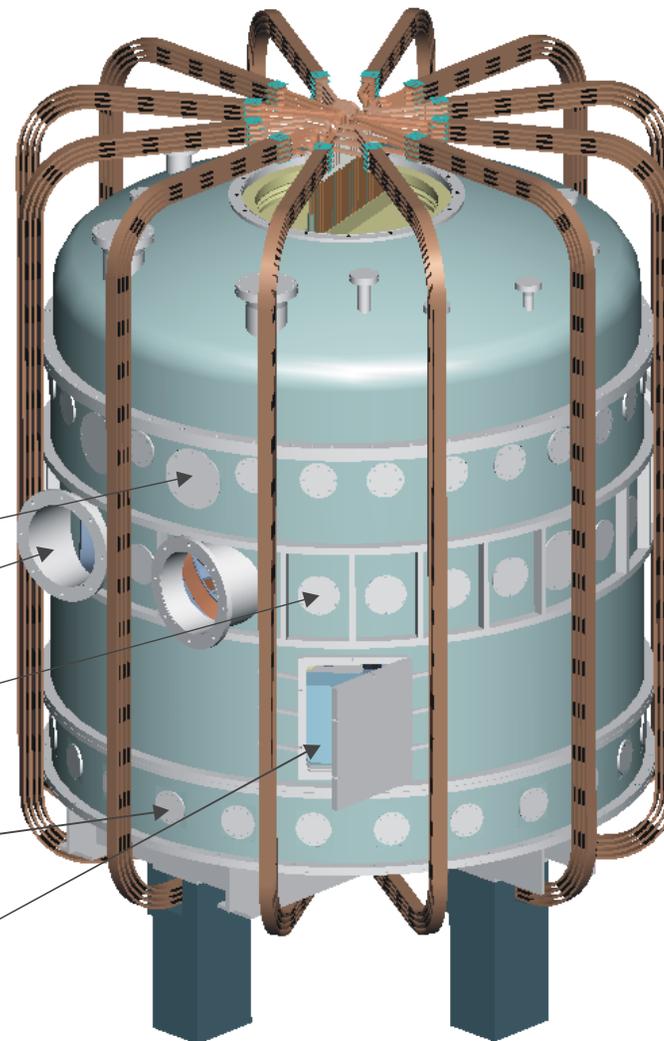
# QPS Access for diagnostics, heating



Plasma

- (6) 12 Dia Ports
- (4) 22 Dia Ports
- (18) 8 Dia Ports
- (23) 6 Dia Ports  
for Coil Leads,  
Coolant Feeds, etc.

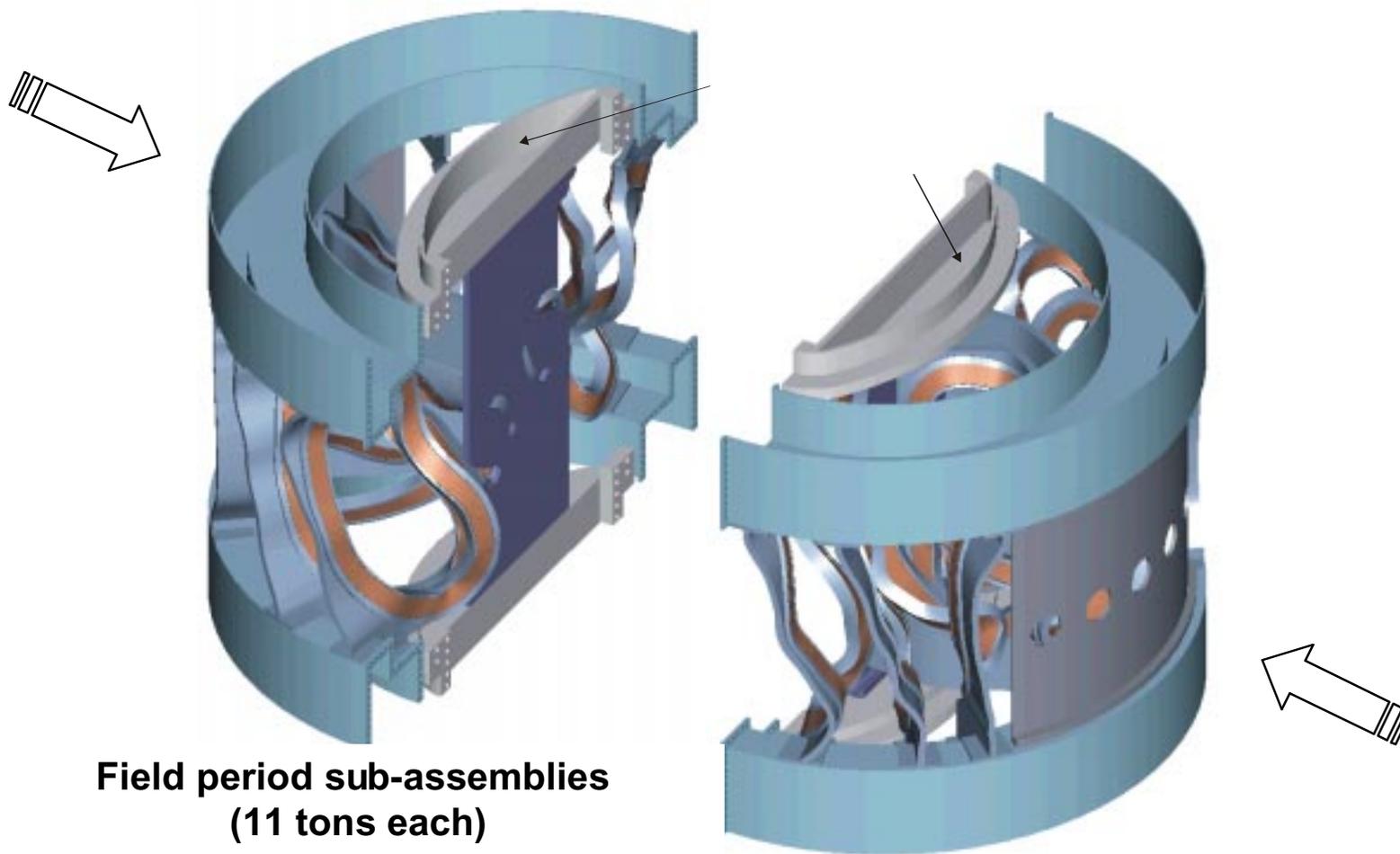
Personnel  
Access Door



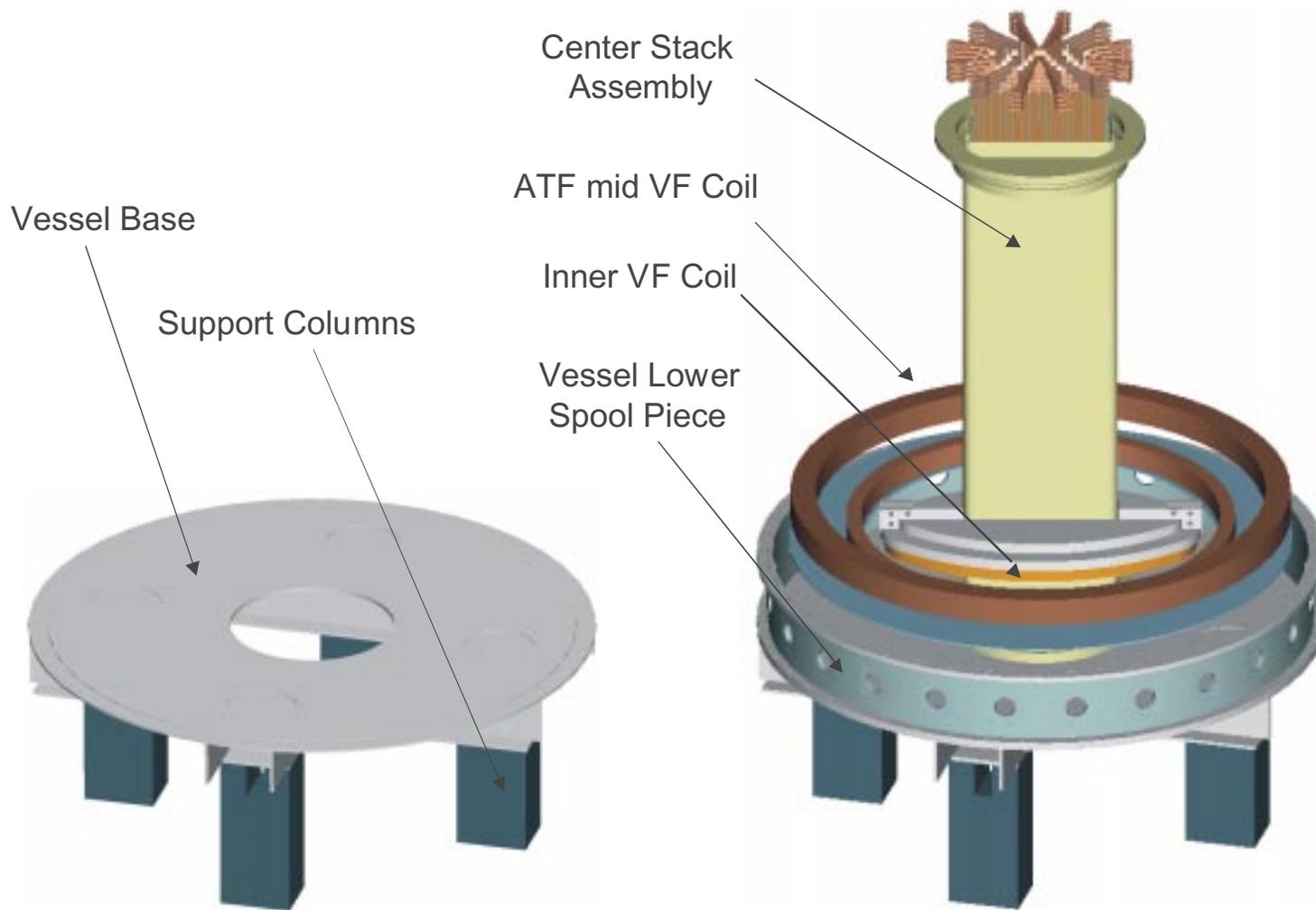
# QPS Assembly

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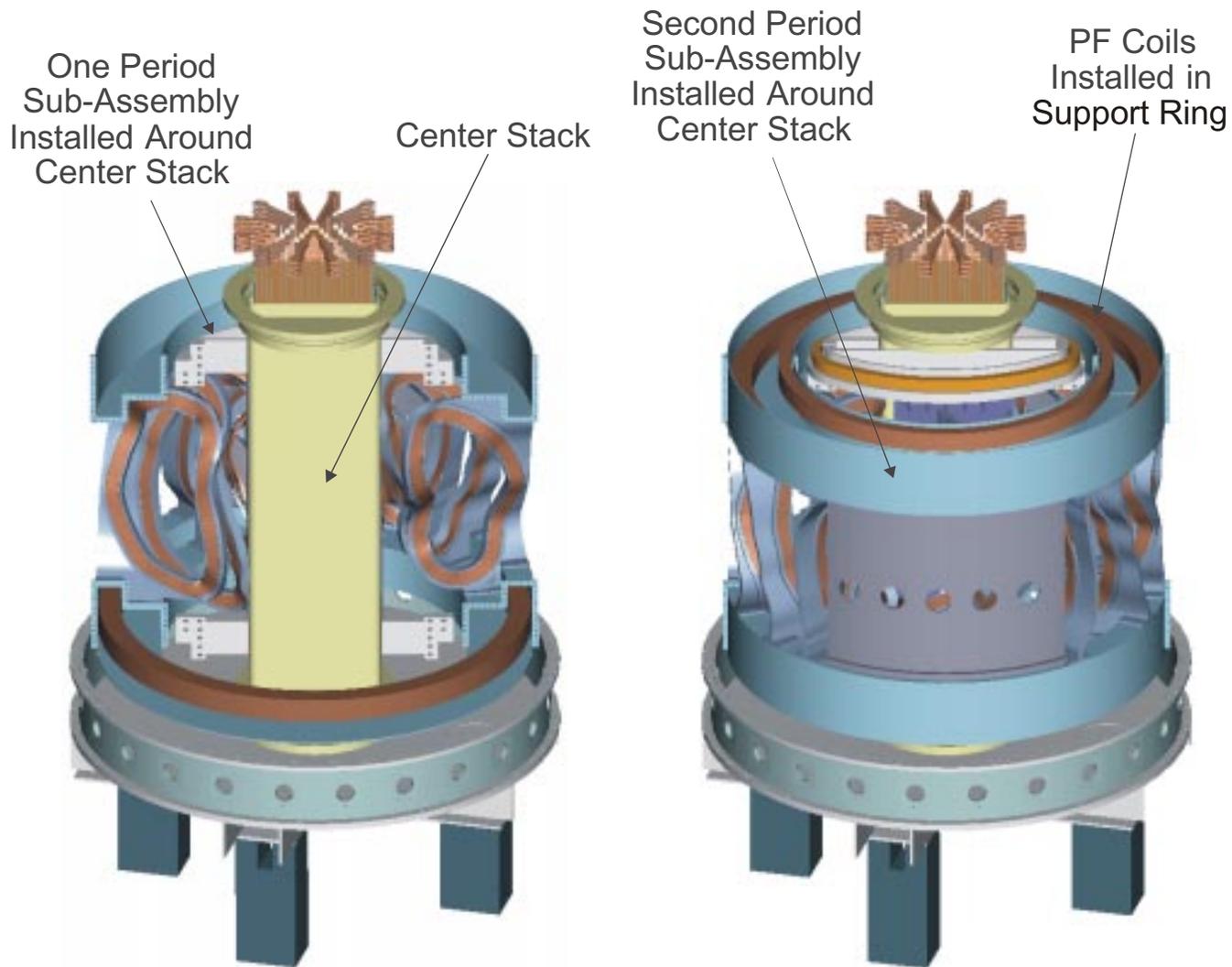
Field periods pre-assembled and fit-checked off site



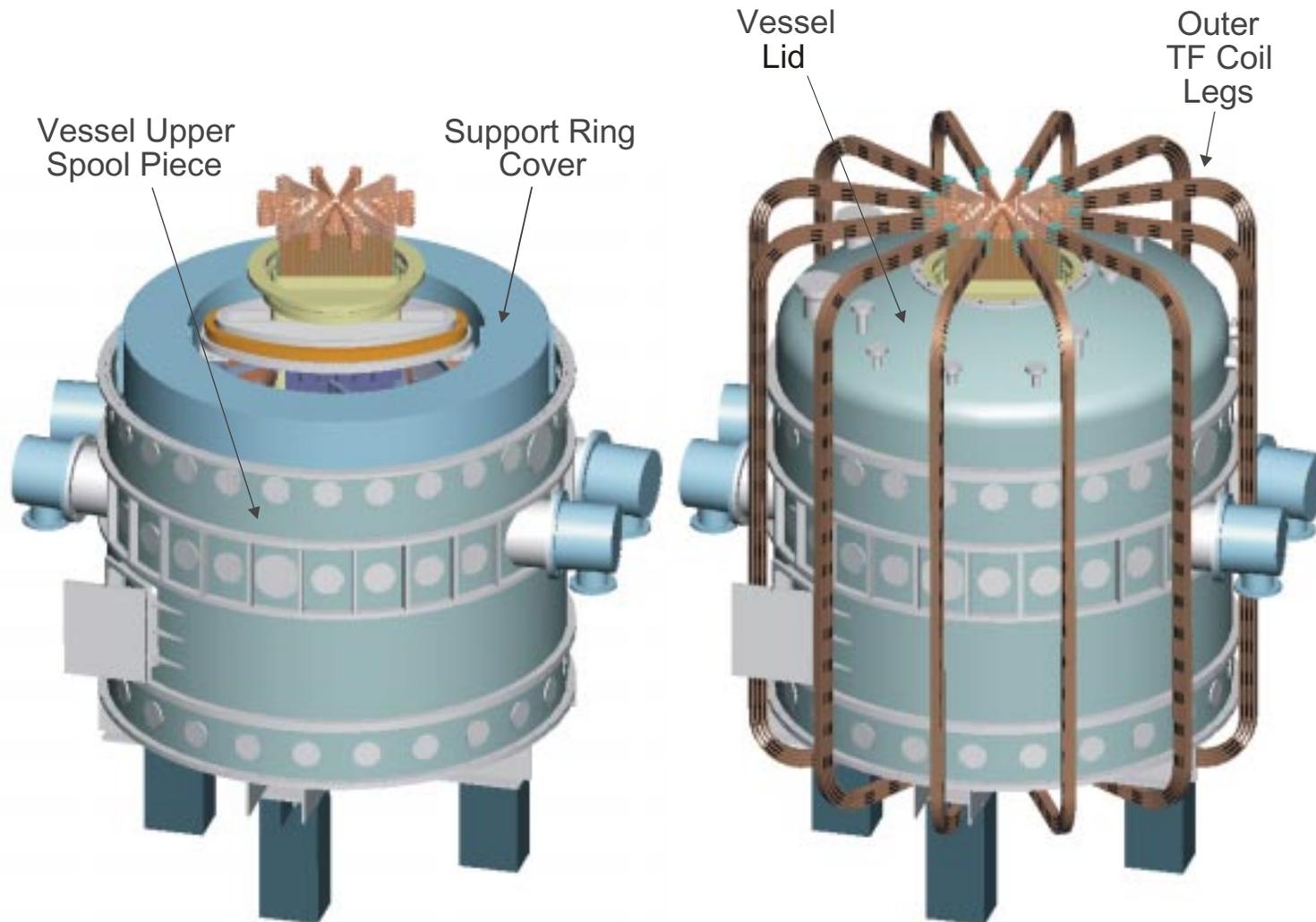
# QPS Assembly sequence (cont d)



# QPS Assembly sequence (cont d)



# QPS Assembly sequence (cont d)



# Conceptual design plans: refine concept, address issues

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- **Improve modular coil geometry**
  - Eliminate sharp bends, optimize twist, reduce current density, improve manufacturability in general
- **Improve structural design**
  - Simplify concept, reduce cost
- **Develop more fabrication details (e.g. castings, windings, canning )**
  - Involve industry and universities to a larger extent
  - Perform manufacturing studies, limited R&D, prototypes
- **Perform tradeoff of OH system**
  - Air core solenoid vs iron core, return coil geometry, etc.
- **Optimize VF coil number, shape, location**
- **Understand consequences of changing VV spool pieces from aluminum to stainless**
- **Finalize design requirements**
- **Develop bottoms up s chedule estimate**
- **Refine cost estimates**

# Summary

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- We have an **initial design concept** that meets performance requirements
  - 16 coil, 2 period modular coil set with integrated structure
  - 0.5 s flat-top at 1 Tesla
  - OH, VF, and TF coil sets
  - External vacuum vessel
- We are making **maximum use of existing equipment** (VF coils, vacuum vessel, etc.) and facilities in order to minimize cost
- We have **plans for improving the design**, by addressing known issues, refining concepts to reduce cost, and updating cost and schedule estimates for a CDR in April 02